Treatment of Dairy Wastewater Effluent Using Submerged Membrane Microfiltration System

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Abstract: Dairy wastewater effluent has become one of the major concerns for the dairy processing industries. Because of large of wastewater effluent generation, the dairy processing industries may become potential candidates for wastewater reuse. Treated wastewater can be utilized in cooling systems and washing plant floor, as well as its potential use for greenery irrigation purposes. In addition, treating dairy effluent will also benefit the environment. The purpose of this study is to characterize wastewater from a selected dairy industry in Kuwait (Kuwait Dairy Company) and a study of applying microfiltration treatment process for treating the dairy wastewater. A complete treatment system including biological treatment, powdered activated carbon (PAC) and submerged membrane microfiltration system (CMF-S) was installed at Kuwait Institute for Scientific Research (KISR) research plant. The overall results of this study indicate that the complete system is capable of treating the dairy effluent. The average removal efficiencies of the system for biological oxygen demand (BOD), chemical oxygen demand (COD), total dissolved solid (TDS) were 98.8%, 92.5%, 96.7% respectively.

Key words: Wastewater, treatment, dairy, membrane.

1. Introduction

In Kuwait, dairy industries are located in the Sulaibiya Agricultural Farm area with no access to the municipal system. The site is under the monitoring by the Environmental Public Authority (EPA), hence, the waste effluent is transported by sewage tankers to the disposal sites in distant parts of the desert. Consequently, disposing untreated dairy wastewater can lead to adverse public health and environmental impacts. Examples of environmental concerns include objectionable odors and fly infestations that have resulted from the disposal of the untreated effluent in open land. Among the food industries, the dairy industry characteristically requires very large quantities of freshwater and generates large quantities of wastewater. Most of the wastewater volume generated in the dairy

industry results from cleaning of transport lines and equipment between production cycles, cleaning of tank trucks, washing of milk silos and equipment malfunctions or operational errors [1-3].

Although the dairy processing industry does not usually deal with extremely hazardous materials, there are many contaminants found in the waste streams that are potentially harmful to the environment. This is particularly true for dairy wastewater which has high concentration of nutrients (nitrate, sulfate and phosphate) along with relatively high BOD, COD and total suspended solid (TSS) [4]. These make the dairy waste unsuitable to be discharged to sewer system or seawater. Recently, the enforcement of environmental legislations is becoming a high priority for the state of Kuwait. Dairy industrial sectors have to comply with the Kuwait Environment Public Authority (KEPA) regulations for wastewater discharge and reuse [5]. To satisfy these regulations, the effluent must be collected and treated to meet the quality standards set by KEPA.

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2. Background

Wastewater treatment systems are designed to eliminate or reduce contaminants to satisfy discharge regulations. There are many methods for treating wastewater generated in dairy industries. Physico-chemical and biological treatment methods are usually used to treat dairy wastewater effluent [2, 3, 6]. However, several studies have found that COD removal is poor in physical-chemical treatment processes and the costs of chemical coagulants are high [7]. On other hand, better organics removal and good effluent quality were reported using biological processes [8]. Among biological treatment processes, treatment in ponds, activated sludge plants and anaerobic treatment are commonly employed for dairy wastewater [9]. In recent years, several works focused on the treatment of dairy effluents demonstrated that application of membrane technologies such as microfiltration (MF), ultrafiltration (UF), nanofiltration (NF) and reverse osmosis (RO) were becoming more energy efficient as compared to conventional methods [10-13].

Membrane technology is based on the principle of selective permeability of one or more components of a liquid mixture through a membrane barrier [14]. In an evaluation of various treatment options for reducing the chemical oxygen demand (COD) of effluents from slaughter house, UF and reverse osmosis processes were more economical than more traditional methods of effluent treatment such as aerobic and anaerobic fermentation and coagulation [15]. The works, that have been dedicated to the treatment of the so-called process waters (flushing waters, first rinse waters or “white waters”), show that nanofiltration (NF) or reverse osmosis (RO) is adequate for the concentration of milk components existed in wastewater stream [16]. The results showed that one single membrane operation allowed the milk constituents to be concentrated in the retentate but reusable water of composition complying with the standard of purified water from process water was not

reached. Integrating two processes such as biological treatment including aeration tank, settling tank and powdered activated charcoal (PAC) with an advanced membrane filtration, may yield a better filtration quality [17]. In this work, the integrated system was used to treat effluent from KD Cow dairy processing plant at Sulaibiya area.

3. Material and Methods

3.1 Material

The complete system for wastewater treatment involves the integration of membrane separation and conventional biological treatment processes. The membrane separation process includes the CMF-S (submerged membrane microfiltration system) which is, a fine filtration process which is a polypropylene membrane filter to remove particles greater than 0.2 μm in size from a feed stream. The MEMCOR® CMF-S process utilizes hollow fiber membranes to provide a self-cleaning system that can maintain high flow rates by the use of a combined air scour and liquid backwash cycle. The membranes are assembled to form a sub-module. This integrated system is shown in Fig. 1, in which feed water passes through an aeration tank for biological treatment. An air compressor injects an adequate air into the aeration tank. The aerobic system includes the process air blowers which are installed adjacent to the system. The required process air flow is $227 \text{ m}^3 \cdot \text{h}^{-1}$ introduced at the bottom of the aerobic tank through air scour distribution header pipes. After passing through the upstream flow, the mixed liquor is transferred by overflow to a suitable buffer flow tank and then pressurized to an operating pressure in accordance with the membrane's design. The specifications of these membrane modules as the following:

- Number of modules: 4;
- Membrane types: Polypropylene;
- Membrane area: 13 m^2 each;
- Filtration direction: outside in;

Fig. 1 Integrated submerged membrane microfiltration system (CMF-S) treatment system.

- Fiber outside diameter: $650\ \mu\text{m} + 30\ \mu\text{m}$;
- Fiber inside diameter: $390\ \mu\text{m} + 20\ \mu\text{m}$;
- Number of fiber: 14,500 nominal;

The treated effluents will flow through PAC to suppress any lactose in the feed effluent and to reduce any odor in the feed water. In the filtration cycle, the membrane tank is filled with feed water to just above the tops of the sub-modules; the inside (filtrate side) of the membranes are then placed under the suction head of the filtrate pump. Filtration takes place from the outer surface of the fiber to the hollow inner core. Feed liquid passes through the porous wall of the fibers, and suspended matter remains on the feed side. This filtration process removes solids larger than approximately $0.2\ \mu\text{m}$. As a guide, bacteria are typically larger than about $1\ \mu\text{m}$. As deposits build up on the fibers, filtration flow resistance increases, resulting in a drop in filtration flow rate. To reduce the flow resistance and restore the filtration flow rate, the membrane is backwashed. During backwash, filtration is stopped and air is applied to the outside of the fibers. A small amount of filtrate is pushed through the fibers (from inside to out) to further remove deposits from the outer surface of the fibers. The tank is then drained to transport any dislodged deposits to the clarifier tank for the separation of any solid particles. The sludge will settle at the bottom of the clarifier. The overflow from the clarifier will be recycled to the aeration tank for further treatment to prevent fermentation of the backwash water.

3.2 Analytical Method

All parameter determinations in the laboratory were performed according to outlined Standard Methods for Water and Wastewater [18]. Both chemical and biological analyses were carried out at the laboratories of Sulaibiya Wastewater Research Plant. Furthermore, the analysis results were cross checked randomly with Kuwait Institute for Scientific Research Central Analytical Laboratory (CAL) as quality assurance.

4. Results and Discussion

4.1 Sampling and Field Measurements

Wastewater within KD Cow dairy processing plant was sampled and monitored on a weekly basis. The samples were collected at points of wastewater outfalls and storage tanks. The type of effluent used in this treatment technique is characterized as dairy industrial wastewater. Dairy refers to a processing plant in which milk or milk-based products are processed into a variety of dairy foods such as milk, cheese, ice cream, sour cream, cream, butter, etc.. It does not include operations in which milk cows are raised and/or milked. Wastewater is primarily washwater resulting from cleaning and sanitizing equipment; thus, it contains some dairy product. Water from general cleanup and hosing down plant facilities ends up in the drains as does rejected fluid from the CIP (cleaning in-place) operations. In addition, product spills of various kinds frequently end up in the floor drains and therefore, become part of the wastewater. The average wastewater generated from KD Cow dairy processing plant is $25.24\ \text{m}^3\cdot\text{h}^{-1}$ which is drained to a waste pit then collected by a wastewater tanker. Table 1 presents the physical and chemical characteristics of the KD Cow effluent, whereas Table 2 presents biological the characteristics of the KD Cow effluent. Table 1 shows the fluctuation in the pH values from 9.64 to 11.25, this is due to the use of CIP in the plant where some detergent or disinfectant has been used. The organic pollutant content of this dairy effluent is commonly expressed as the BOD_5 and COD. As seen in Table 2, the concentrations of BOD and COD in the dairy processing effluents vary widely, from $80\ \text{mg}\cdot\text{L}^{-1}$ to $246\ \text{mg}\cdot\text{L}^{-1}$ and $216\ \text{mg}\cdot\text{L}^{-1}$ to $431\ \text{mg}\cdot\text{L}^{-1}$, respectively.

4.2 Operating and Optimizing the Pilot Unit

During the period of this task, the integrated treatment system was operated and tested on a daily

Table 1 Physical and chemical characteristics of the KD cow effluent

Parameters	Average	Max	Min
TDS (Total dissolved solid) ($\text{mg}\cdot\text{L}^{-1}$)	997.2	1,075	944
Electrical conductivity ($\mu\text{S}\cdot\text{cm}^{-1}$)	1,356.6	1,605	1,072
pH	10.072	11.25	9.64
Total Alkalinity ($\text{mg}\cdot\text{L}^{-1}$ as CaCO_3)	186.3	199	173
Ca^{+} ($\text{mg}\cdot\text{L}^{-1}$ as CaCO_3)	14.475	16.2	13.8
Mg^{+} ($\text{mg}\cdot\text{L}^{-1}$)	5.737	6.3	4.98
SO_4^{-} ($\text{mg}\cdot\text{L}^{-1}$)	124.25	162	113
Cl^{-} ($\text{mg}\cdot\text{L}^{-1}$)	377.4	382.15	370.67
NTU (turbidity)	233.5	475	82
TSS ($\text{mg}\cdot\text{L}^{-1}$)	99.25	131	65
$\text{NH}_3\text{-N}$ ($\text{mg}\cdot\text{L}^{-1}$)	2.3755	2.91	1.01
NO_3^{-} ($\text{mg}\cdot\text{L}^{-1}$)	79.30	87.1	51.62
PO_4^{-} ($\text{mg}\cdot\text{L}^{-1}$)	6.5125	7.87	5.02

* The presented values represent a total of 20 samples.

Table 2 Biological characteristics of the KD cow effluent

Parameter	Average	Max	Min
BOD_5 ($\text{mg}\cdot\text{L}^{-1}$)	160.05	246	80
COD ($\text{mg}\cdot\text{L}^{-1}$)	257.7	431	216
Fecal Coliform Bacteria (colonies/100 mL)		0	0
Oil & Grease (ppm)	26.13	56.81	2.57

* The presented values represent a total of 20 samples.

basis and operating parameters, such as pH, temperature, feed pressure, flow rate, feed conductivity and turbidity, were monitored and recorded daily. The graphical presentations of the data recorded daily for the turbidity and TMP (trans-membrane pressure) appear in Figs. 2 and 3. The temperature of the feedwater to the system ranged between 24.90°C and 41.30°C , during winter and summer respectively (Fig. 4). The pH of the feedwater during this period was between 6.06 and 12.17 (Fig. 5). Feed and filtrate turbidity values ranged from 6.59 NTU to 429 NTU and from 0.09 NTU to 17.42 NTU, respectively (Fig. 3). The turbidity measuring unit is Nephelometric Turbidity Unit (NTU) as recommended by the filter manufacturer. The conductivity of the feed water was also monitored and was found to be between $79.9\mu\text{S}\cdot\text{cm}^{-1}$ (micro Siemens per cm) and $3,610\mu\text{S}\cdot\text{cm}^{-1}$ during the monitoring

period as presented in Fig. 6. The conductivity measuring unit is $\mu\text{S}\cdot\text{cm}^{-1}$ as recommended by the membrane manufactures. At the beginning of the experimental testing program, the pilot system was tested under variable operating conditions to determine the optimal operating conditions of the system.

During commissioning period, operating parameters were optimized to achieve best performance of the biological treatment system. The optimized parameters were flowrate, HRT (hydraulic retention time), SRT (sludge retention time), DO (dissolved oxygen) and MLSS (mixed liquor suspended solids). The biological treatment system was operated with aerobic (capacity 6m^3) and anoxic (capacity 6m^3) tanks, and with a flux range of $14\text{L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$ to $24\text{L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$ and an HRT of 2 h. The system was operated without activated sludge wasting to allow the MLSS to

Fig. 2 Transmembrane pressure (TMP) versus running hours.

Fig. 3 Raw, feed and filtrate turbidity versus running hours.

increase in the aeration tank. The sludge wasting rate was set to give an SRT in the range of 34 h to 47 h. The average TSS recorded in the aeration tank was $120 \text{ mg}\cdot\text{L}^{-1}$, with maximum and minimum values of $274 \text{ mg}\cdot\text{L}^{-1}$ and $10 \text{ mg}\cdot\text{L}^{-1}$, respectively. The SRT values are presented in Fig. 7. The DO concentrations in the biological treatment ranged from $2.0 \text{ mg}\cdot\text{L}^{-1}$ to $2.7 \text{ mg}\cdot\text{L}^{-1}$ and from $0.1 \text{ mg}\cdot\text{L}^{-1}$ to $0.7 \text{ mg}\cdot\text{L}^{-1}$, in the

aerobic and anoxic tanks, respectively (Fig. 8). It is worth mentioning that during the operation there were negligible amount of sludge and surface foam recovered from the settling tank compared to the amounts of flowrate to the system.

4.3 Quality Analysis

The results of all analyses are summarized in Table 3

Fig. 4 Raw wastewater temperature versus running hours.

Fig. 5 Raw water pH versus running hours.

representing the chemical analysis of maximum, minimum and average of raw water, feed water, and filtrate water. While Table 4 presents the removal efficiencies of the integrated treatment system in reducing the BOD, COD, and TSS. Figs. 9, 10 and 11 show graphic presentation of the performance for the

system in term of the reduction of values of COD, BOD and TSS, respectively. Chemical analyses of all samples indicate that the integrated treatment system had no significant effect on other constituents of the dairy effluent wastewater such as phosphate, Mg^{+} , Ca^{+} and electrical conductivity (EC). The analysis shows

Fig. 6 Feedwater conductivity versus running hours.

Fig. 7 Solid retention time of the biological treatment system.

that the integrated treatment system can reduce BOD by up to 98.8%, COD by up to 92.5% and TSS by up to 96.7% (Table 4). This reflects the excellent efficiency of both the CMF-S and the biological treatment including the aeration tank and the activated carbon filter in removing biological matter and suspended materials from the dairy effluent

wastewater.

4.4 COD and BOD.

The COD and BOD measurements of feedwater and integrated (CMF-S) treatment system filtrate are shown in Figs. 9 and 10 respectively. The influent COD and BOD highly fluctuated during the period of

Fig. 8 Dissolved oxygen versus running hours for aeration and anoxic tanks.

Table 3 Chemical analysis of raw water, feed water and filtrate water.

Parameters	Raw Water			Feed Water			Filtrate Water		
	Max	Min	Ave	Max	Min	Ave	Max	min	Ave
pH	12.35	6.10	10.38	11.80	6.85	8.86	11.73	7.08	8.73
EC ($\mu\text{S}\cdot\text{cm}^{-1}$)	3,940.00	693.00	2,029.22	3,580.00	864.00	1,841.11	2,570.00	782.00	1,667.67
TSS ($\text{mg}\cdot\text{L}^{-1}$)	638.00	21.00	281.00	274.00	10.00	128.00	35.20	1.00	9.00
NTU	527	103	300.8	496	6.6	128.7	18	0.04	3.3
TDS ($\text{mg}\cdot\text{L}^{-1}$)	2,276.00	564.00	1,419.00	3,118.00	639.00	1,315.54	1,956.00	614.00	1,187.47
Cl^{-} ($\text{mg}\cdot\text{L}^{-1}$)	269.00	70.00	120.62	295.00	60.00	151.92	285.00	40.00	138.27
Total Alkalinity ($\text{mg}\cdot\text{L}^{-1}$)	972.00	66.00	457.14	1,554.00	206.00	602.81	1,220.00	156.00	579.47
PO_4^{-} ($\text{mg}\cdot\text{L}^{-1}$)	22.52	2.76	9.71	17.39	2.09	6.34	6.98	1.53	3.54
Ca^{+} ($\text{mg}\cdot\text{L}^{-1}$)	0.53	0.01	0.18	0.39	0.01	0.10	0.07	0.00	0.03
Mg^{+} ($\text{mg}\cdot\text{L}^{-1}$)	2.45	1.54	1.91	2.33	0.47	1.41	1.90	0.28	1.12
Pb^{+} ($\text{mg}\cdot\text{L}^{-1}$)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Cd^{+} ($\text{mg}\cdot\text{L}^{-1}$)	0.43	0.01	0.08	0.04	0.00	0.02	0.04	0.00	0.02
Zn^{+} ($\text{mg}\cdot\text{L}^{-1}$)	0.44	0.05	0.14	0.13	0.02	0.06	0.06	0.00	0.02
Ni^{+} ($\text{mg}\cdot\text{L}^{-1}$)	0.02	0.00	0.01	0.01	0.00	0.01	0.01	0.00	0.00

* The presented values represent a total of 115 samples.

operation and were in the range of from 26-1,237 $\text{mg}\cdot\text{L}^{-1}$ and 569-1,208 $\text{mg}\cdot\text{L}^{-1}$, respectively. COD concentration in the effluent was varied from 1.3-36 $\text{mg}\cdot\text{L}^{-1}$ with an average value of 9 $\text{mg}\cdot\text{L}^{-1}$. Whereas, the majority of BOD values of the integrated system filtrate were less than 8 $\text{mg}\cdot\text{L}^{-1}$, with an average value

of 3.2 $\text{mg}\cdot\text{L}^{-1}$. Table 4 presents the removal efficiencies for BOD, COD and TSS. The average removal efficiencies of the system for BOD, chemical oxygen demand COD were 98.8% and 92.5%, respectively. This significant reductions in both COD and BOD values reveal that the heterotrophic bacteria

Table 4 Average removal efficiencies of the integrated treatment system.

Parameters	Removal efficiency (%)
TSS	96.7
COD (mg/L)	92.5
BOD (mg/L)	98.8

which is responsible of degrading the carbonaceous organic is rich in aerobic zone of the system. These results also show that the integrated system can provide a consistently high organic removal efficiency during continuous long time of operation.

5. Conclusion

Based on the results of this study, the following conclusions are made:

The performance of the integrated treatment system is capable of treating the dairy wastewater effluent and producing good filtrate water with an average turbidity of 3.3 NTU clear of most impurities.

The average removal efficiencies of the integrated treatment system for BOD, COD and TSS are 98.8%, 92.5% and 96.7%, respectively.

Fig. 9 COD measurements of raw, feed water and filtrate. **Fig. 10** BOD measurements of raw, feed water and filtrate.

Fig. 11 TSS measurements of raw, feed water and filtrate.

The chemical analysis revealed that both biological and CMF-S systems can significantly improved the quality of dairy wastewater effluents. Therefore, water produced from the both systems could be considered to be safe for agriculture, industry and other indirect human uses.

The final filtrate of the system is suitable for further polishing with RO (reverse osmosis) system for a further improved water quality.

The system demonstrates an excellent operational availability under prevalent conditions of Kuwait which is 90.39%.

The characteristics of water produced from the integrated system are better than the standard for water reusing in landscaping.

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References

- [1] Askaran, K. B., Palmowski, L. M., and Watson, B. M. 2003. "Wastewater Reuse and Treatment Options for the Dairy Industry." *Water Science and Technology* 3: 85-91.
- [2] Danalewich, J. R., Papagiannis, T. G., Belyea, R. L., Tumbleson, and Raskin, M. E. L. 1998. "Characterization of Dairy Waste Streams, Current Treatment Practices, and Potential for Biological Nutrient Removal." *Water Research* 32: 3555-3568.
- [3] Vidal, G., Carvalho, A., Mendez, R., and Lema J. M. 2000. "Influence of the Content in Fats and Proteins on the Anaerobic Biodegradability of Dairy Wastewaters." *Bio-resource Technology* 74 : 231-239.
- [4] Green, M., Gidron, E., Beliaevski, M., Lahav, O., and Tarre, S. 2004. "Treatment of Dairy Wastewater using a Vertical Bed with Passive Aeration." *Environmental Technology* 25 (10): 1123-1130.
- [5] Environmental Public Authority Kuwait (EPA), 2001. Wastewater Criteria for Disposal in State of Kuwait.
- [6] Kasapgil, B., Anderson, G. K., and Ince, O. 1994. "An Investigation into the Pretreatment of Dairy Wastewater Prior to Aerobic Biological Treatment." *Water Science Technology* 29: 205-212.
- [7] Sharma, D. 2014. "Treatment of Dairy Waste Water by Electro Coagulation using Aluminum Electrodes and Settling, Filtration Studies." *International Journal of Chemical Technolgy Research* 6 (1): 591-599.

- [8] Bangsbo, D., Hansen, I. 1985. "Treatment of Dairy Wastewater in the Developing Countries—the Danish Experience." *India Environment* 8: 2-10.
- [9] Demirel, B., Yenigun, O., and Onay, T. T. 2005. "Anaerobic Treatment of Dairy Wastewaters." *Process Biochemistry* 40: 2583-2595.
- [10] Mavrov, V., Chmiel, H., and Belieres, E. 2001. "Spent Process Water Desalination and Organic Removal by Membranes for Water Reuse in the Food Industry." *Desalination* 138: 65-74.
- [11] Yip, V., Arnsfield, S.D., and Hydamaka, A.W. 1996. "Potential for Stainless Steel Microfiltration Processing to Reduce Effluent from a Fluid Milk and Ice Cream Processing Plant." *Journal of Dairy Science* 79: 710-716.
- [12] Blanchard, B. D. 1991. "Plant Effluents Dairy Waste Streams Recovery." *Dairy, Food and Environmental Sanitation* 11 (9): 494-496.
- [13] Koyuncu, I., Turan, M., Topacik, D., and Ates, A. 2000. "Application of Low Pressure Nanofiltration Membranes for the Recovery and Reuse of Dairy Industry Effluents." *Water Science and Technology* 41: 213-221.
- [14] Jelen, P. 1991. "Pressure-Driven Membrane Processes: Principles and Definitions." International Dairy Federation, Brussels, Belgium.
- [15] Cowan, J. A. C., MacTavish, F., Brouckaert, C. J., and Jacobs E. P. 1992. "Membrane Treatment Strategies for Red Meat Abattoir Effluents." *Water Science and Technology* 25 (10): 137-148.